

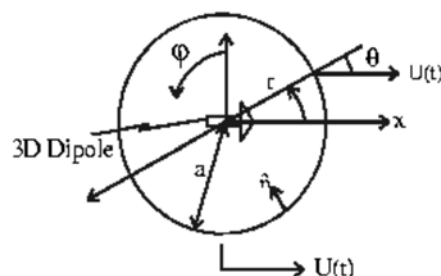
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### 3.11 Unsteady Motion - Added Mass

**D'Alembert:** ideal, irrotational, unbounded, steady.

Example 1: Force on a sphere accelerating ( $\mathbf{U} = \mathbf{U}(t)$ , unsteady) in an unbounded fluid at rest. (at infinity)



K.B.C on sphere:  $\frac{\partial \phi}{\partial r} \Big|_{r=a} = U(t) \cos \theta$

Solution: Simply a 3D dipole (no stream)

$$\phi = -U(t) \frac{a^3}{2r^2} \cos \theta$$

Check:  $\frac{\partial \phi}{\partial r} \Big|_{r=a} = U(t) \cos \theta$

Hydrodynamic force:

$$F_x = -\rho \iint_B \left( \frac{\partial \phi}{\partial t} + \frac{1}{2} |\nabla \phi|^2 \right) n_x dS$$

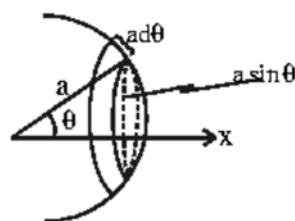
On  $r = a$ :

$$\frac{\partial \phi}{\partial r} \Big|_{r=a} = -\dot{U} \frac{a^3}{2r^2} \cos \theta \Big|_{r=a} = -\frac{1}{2} \dot{U} a \cos \theta$$

$$\nabla \phi \Big|_{r=a} = \left( U \cos \theta, \frac{1}{2} U \sin \theta, 0 \right) \quad V_r = \frac{\partial \phi}{\partial r} = \frac{1}{r} \frac{\partial \phi}{\partial \theta} = \frac{1}{r \sin \theta} \frac{\partial \phi}{\partial \varphi}$$

$$|\nabla \phi|^2 \Big|_{r=a} = U^2 \cos^2 \theta + \frac{1}{4} U^2 \sin^2 \theta; \hat{n} = -\hat{e}_r, n_x = -\cos \theta$$

$$\iint_B dS = \int_0^\pi (a d\theta) (2\pi a \sin \theta)$$



Finally,

$$\begin{aligned}
 F_x &= (-\rho) 2\pi a^2 \int_0^\pi d\theta (\sin \theta) \underbrace{\left( -\cos \theta \right)}_{n_x} \left[ \underbrace{-\frac{1}{2} \dot{U} a \cos \theta}_{\frac{\partial \phi}{\partial t}} + \frac{1}{2} \underbrace{\left( U^2 \cos^2 \theta + \frac{1}{4} U^2 \sin^2 \theta \right)}_{|\nabla \phi|^2} \right] \\
 &= -\pi \rho \dot{U} a^3 \underbrace{\int_0^\pi d\theta \sin \theta \cos^2 \theta}_{2/3} + \rho U^2 \pi a^2 \underbrace{\int_0^\pi d\theta \sin \theta \cos \theta \left( \cos^2 \theta + \frac{1}{4} \sin^2 \theta \right)}_{=0 \text{ D'Alembert revisited}} \\
 F_x &= -\dot{U}(t) \left[ \underbrace{\rho \frac{2}{3} \pi a^3}_{\text{unit: mass}} \right] \quad F_x = 0 \text{ if } \dot{U} = 0 \text{ steady (D'Alembert's Condition)}
 \end{aligned}$$

### General 6 degrees of freedom motions

#### Added mass matrix (tensor)

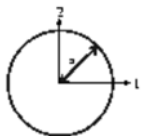
$$m_{ij} ; i, j = \underbrace{1, 2, 3}_{\dot{u}, \dot{v}, \dot{w}} \quad \underbrace{4, 5, 6}_{\dot{\Omega}_x, \dot{\Omega}_y, \dot{\Omega}_z}$$

$m_{ij}$ : associated with force on body in  $i$  direction due to unit acceleration in  $j$  direction. For example, for a sphere:

$$m_{11} = m_{22} = m_{33} = \frac{1}{2} \rho \forall = (m_A) \quad \text{all other } m_{ij} = 0$$

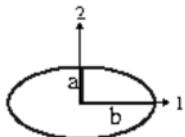
#### Some added masses of simple 2D geometries

- circle figure



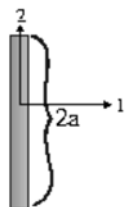
$$m_{11} = m_{22} = \rho \forall = \rho \pi a^2$$

- ellipse figure



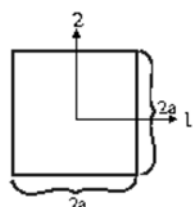
$$m_{11} = \rho \pi a^2, m_{22} = \rho \pi b^2$$

- plate figure



$$m_{11} = \rho \pi a^2, m_{22} = 0$$

- square figure

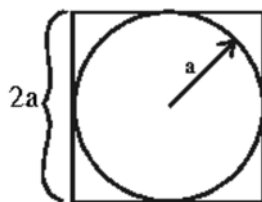


$$m_{11} = m_{22} \approx 4.754 \rho a^2$$

A reasonable estimate for added mass of a 2D body is to use the displaced mass ( $\rho V$ ) of an "equivalent cylinder" of the same lateral dimension or one that "rounds off" the body. For example, we consider a square:

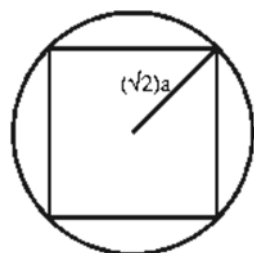
1.

inscribed circle:  $m_A = \rho \pi a^2 = 3.14 \rho a^2$ .



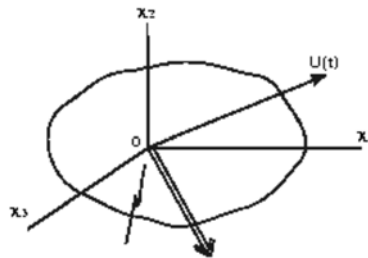
2.

circumscribed circle:  $m_A = \rho \pi (\sqrt{2}a)^2 = 6.28 \rho a^2$ .



Arithmetic mean of 1) + 2)  $\approx 4.71 \rho a^2$ .

General 6 degrees of freedom forces and moments on a rigid body moving in an unbounded fluid ( at rest at infinity)



$$\vec{U}(t) = (U_1, U_2, U_3) \quad \text{Translation velocity}$$

$$\vec{\Omega}(t) = (\Omega_1, \Omega_2, \Omega_3) \equiv (U_4, U_5, U_6) \quad \text{Rotation (velocity) with respect to O}$$

Note:  $OX_1X_2X_3$  fixed in the body.

Then (JNN §4.13)

- forces

$$F_j = -\dot{U}_i m_{ji} - E_{jkl} U_i \Omega_k m_{li} \quad \text{with } i = 1, 2, 3, 4, 5, 6 \text{ and } j, k, l = 1, 2, 3$$

- moments

$$M_j = -\dot{U}_i m_{j+3,i} - E_{jkl} U_i \Omega_k m_{l+3,i} - E_{jkl} U_k U_i m_{li} \quad \text{with } i = 1, 2, 3, 4, 5, 6 \text{ and } j, k, l = 1, 2, 3$$

Einstein's  $\Sigma$  notation applies.

$$E_{jkl} = \text{"alternating tensor"} = \begin{cases} 0 & \text{if any } j, k, l \text{ are equal} \\ 1 & \text{if } j, k, l \text{ are in cyclic order, i.e., } (1, 2, 3), (2, 3, 1), \text{ or } (3, 1, 2) \\ -1 & \text{if } j, k, l \text{ are not in cyclic order i.e., } (1, 3, 2), (2, 1, 3), (3, 2, 1) \end{cases}$$

Note:

1.

if  $\Omega_k \equiv 0$ ,  $F_j = -\dot{U}_i m_{ji}$  (as expected by definition of  $m_{ij}$ ). Also if  $\dot{U}_i \equiv 0$ , then  $F_j = 0$  for any  $U_i$ , no force in steady translation.

2.

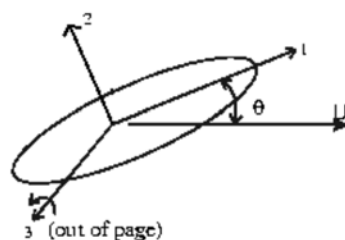
$B_i \sim U_i m_{ii}$  "added momentum" due to rotation of axes, 2)  $\sim \vec{\Omega} \times \vec{B}$  where  $\vec{B}$  is linear momentum. (momentum from 1 coordinate into new  $x_j$  direction)

3.

$$\text{If } \Omega_k \equiv 0 : M_j = \underbrace{-\dot{U}_i m_{j+3,i} m_{ij}}_{\text{def. of}} - \underbrace{E_{jkl} U_k U_i m_{li}}_{\text{even with } \dot{U}=0, M_j \neq 0 \text{ due to this term}}$$

Moment on a body due to pure steady translation - "Munk" moment.

**Example of Munk Moment - a 2D submarine in steady translation**



$$U_1 = U \cos \theta$$

$$U_2 = -U \sin \theta$$

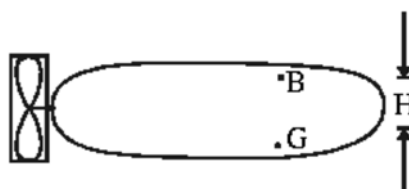
Consider steady motion:  $\dot{U} = 0$ ;  $\Omega_k = 0$ . Then

$$M_3 = -E_{3kl} U_k U_l m_{li}$$

For a 2D body,  $m_{3i} = m_{i3} = 0$ , also  $U_3 = 0, i, k, l = 1, 2$ . This implies that:

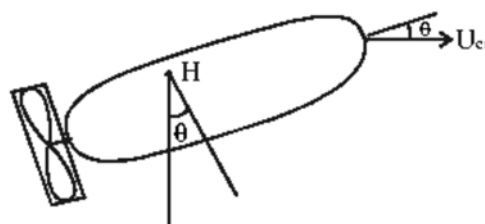
$$\begin{aligned} M_3 &= -\underbrace{E_{312}}_{=1} U_1 (U_1 m_{21} + U_2 m_{22}) - \underbrace{E_{321}}_{=-1} U_2 (U_1 m_{11} + U_2 m_{12}) \\ &= -U_1 U_2 (m_{22} - m_{11}) \\ &= U^2 \sin \theta \cos \theta \left( \underbrace{m_{22} - m_{11}}_{>0} \right) \end{aligned}$$

Therefore,  $M_3 > 0$  for  $0 < \theta < \pi/2$  ("Bow up"). Therefore, a submarine under forward motion is unstable in pitch (yaw) (e.g., a small bow-up tends to grow with time), and control surfaces are needed:



- Restoring moment  $\approx (\rho g \nabla) H \sin \theta$ .
- [critical speed](#)  $U_{cr}$  given by:

$$(\rho g \nabla) H \sin \theta \geq U_{cr}^2 \sin \theta \cos \theta (m_{22} - m_{11})$$



Usually  $m_{22} \gg m_{11}$ ,  $m_{22} \approx \rho \nabla$ . For small  $\theta$ ,  $\cos \theta \approx 1$ . So,  $U_{cr}^2 \leq gH$  or  $F_{cr} \equiv \frac{U_{cr}}{\sqrt{gH}} \leq 1$ . Otherwise, control fins are required.

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