

Dinghy 13 'Bump' version

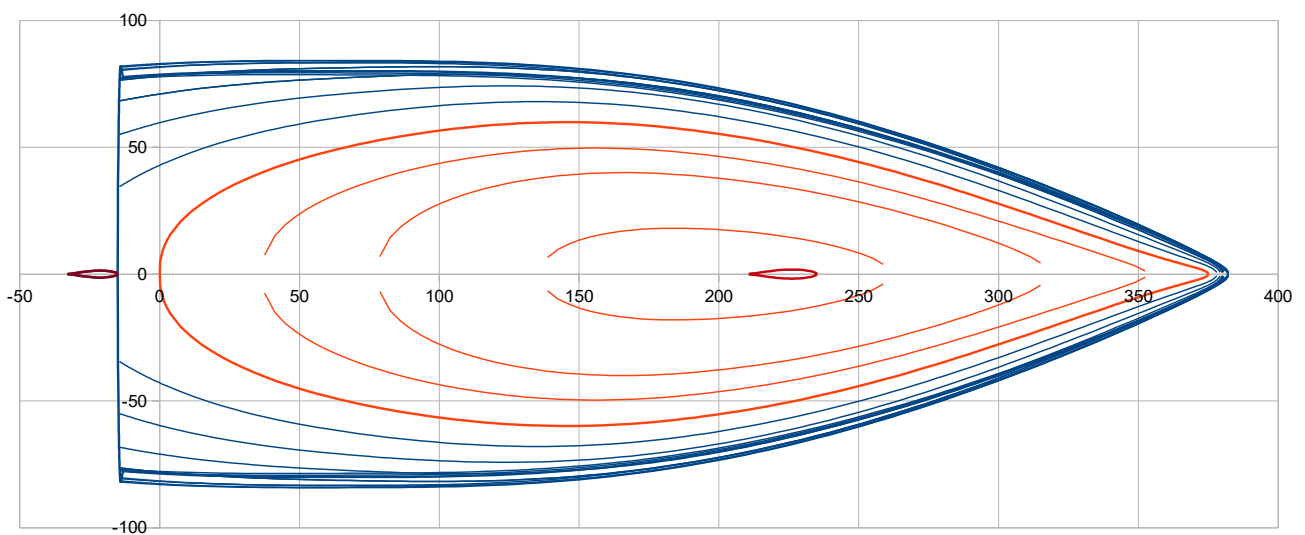
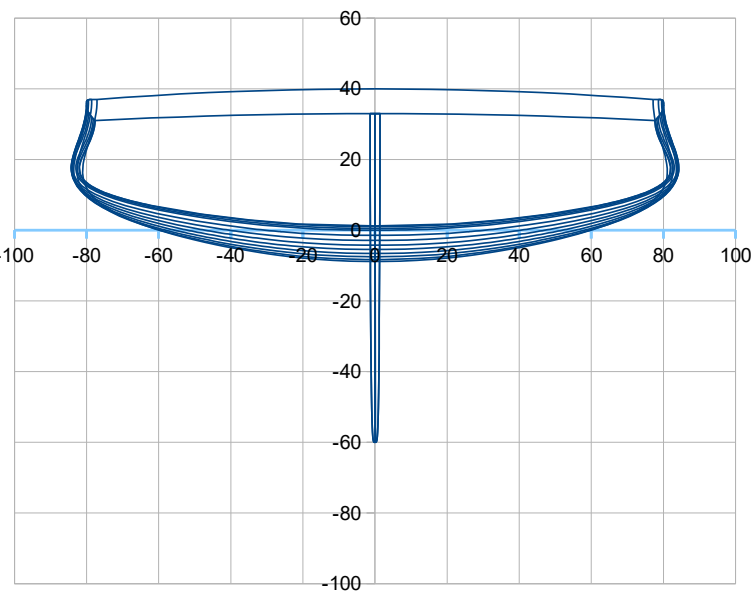
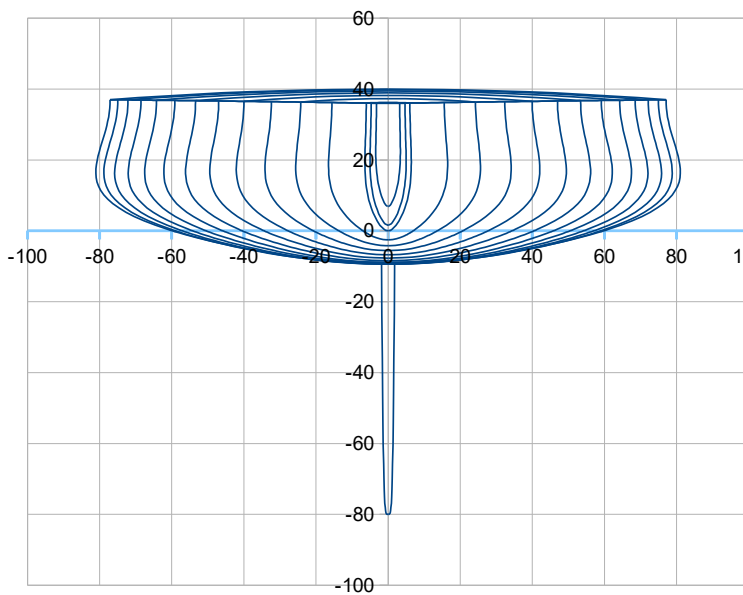
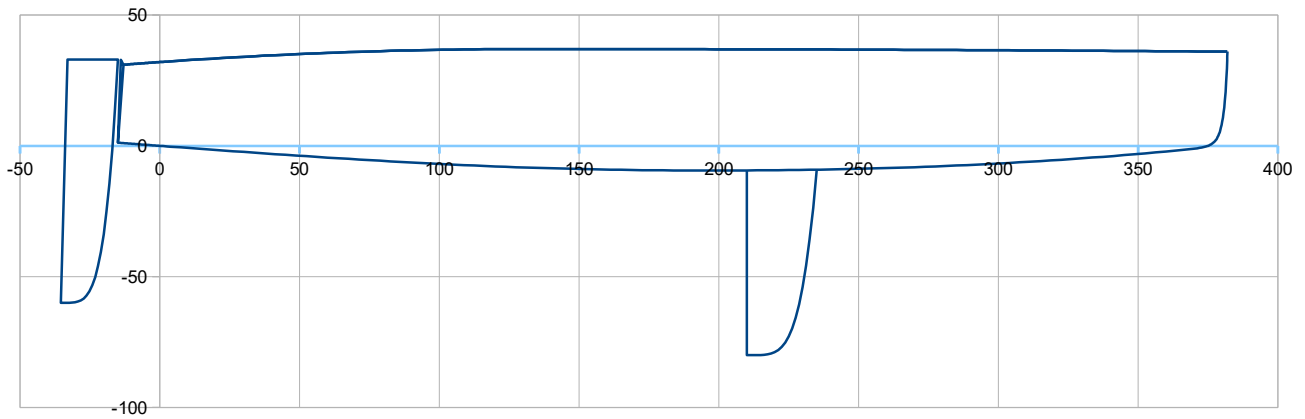
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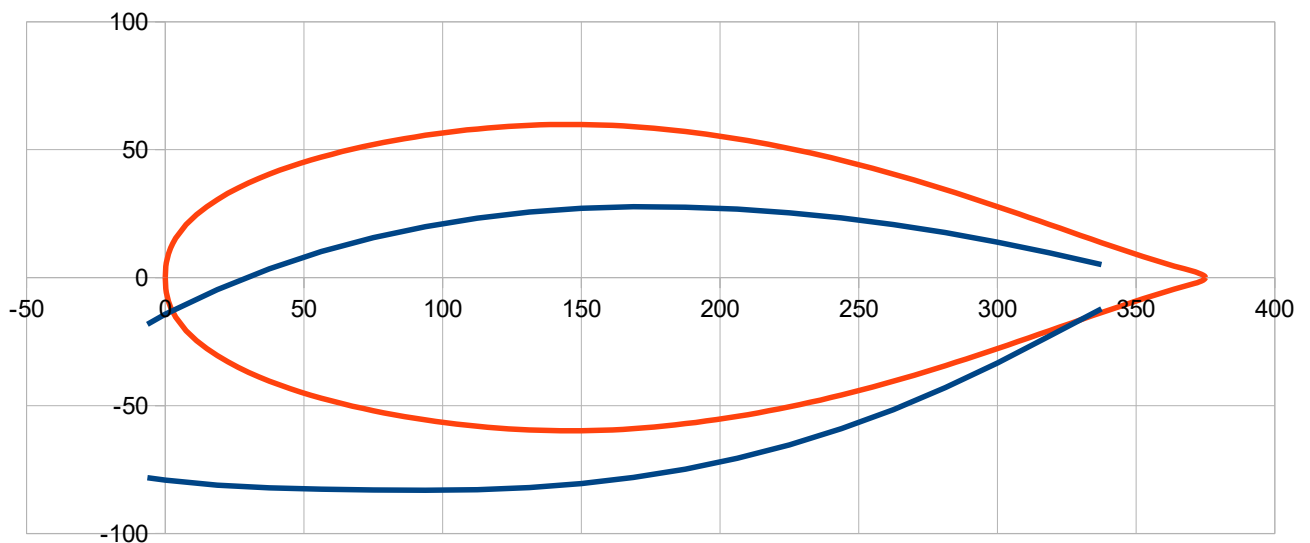
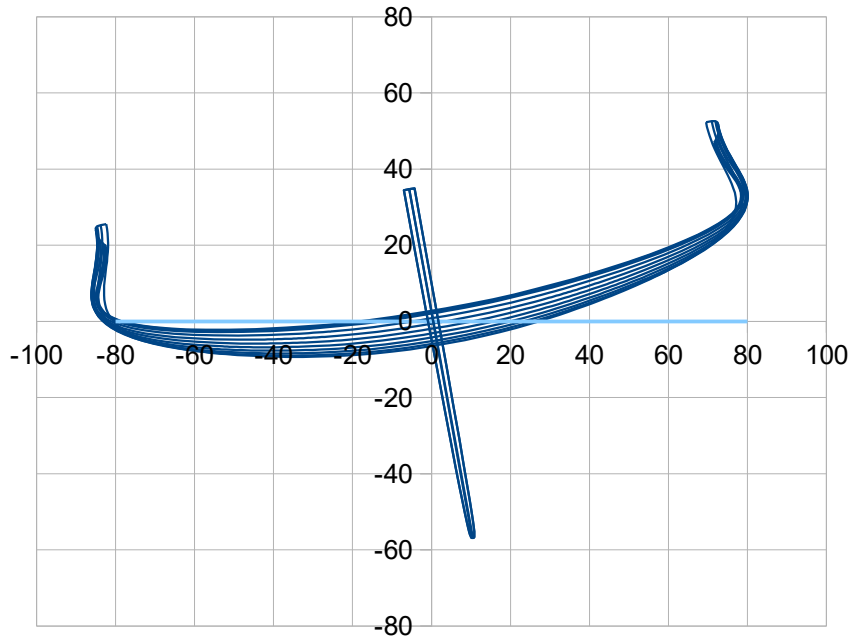
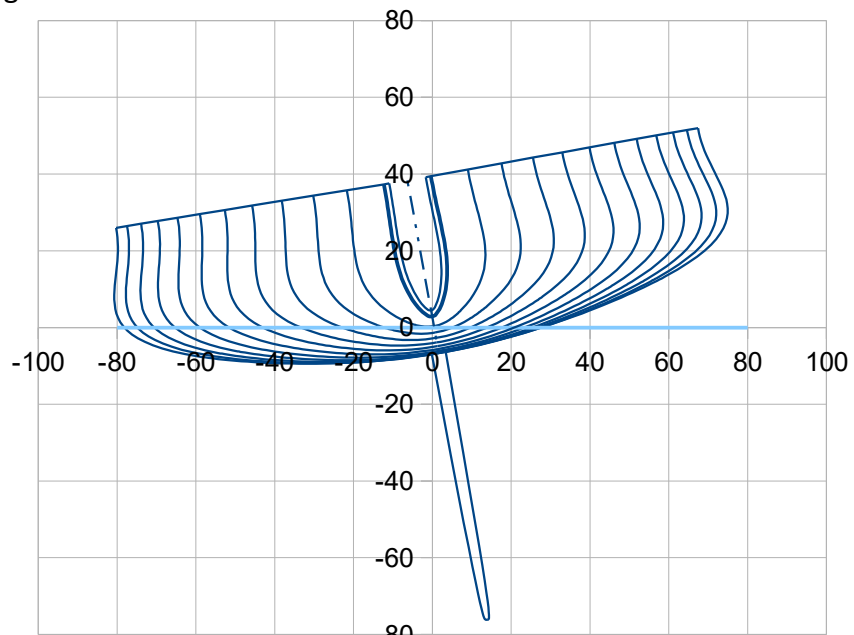
Lhull : 3,97 m (13 ft) ; Bhull : 1,60 m (at sheer line) ; Light weight assumed 61 kg (with a 8 m² sail)

With the design « payload » 95 kg (a heavy helmsman case) :

>>> Lwl : 3,75 m ; Bwl : 1,20 m >>> Bwl / Bhull = 0,749



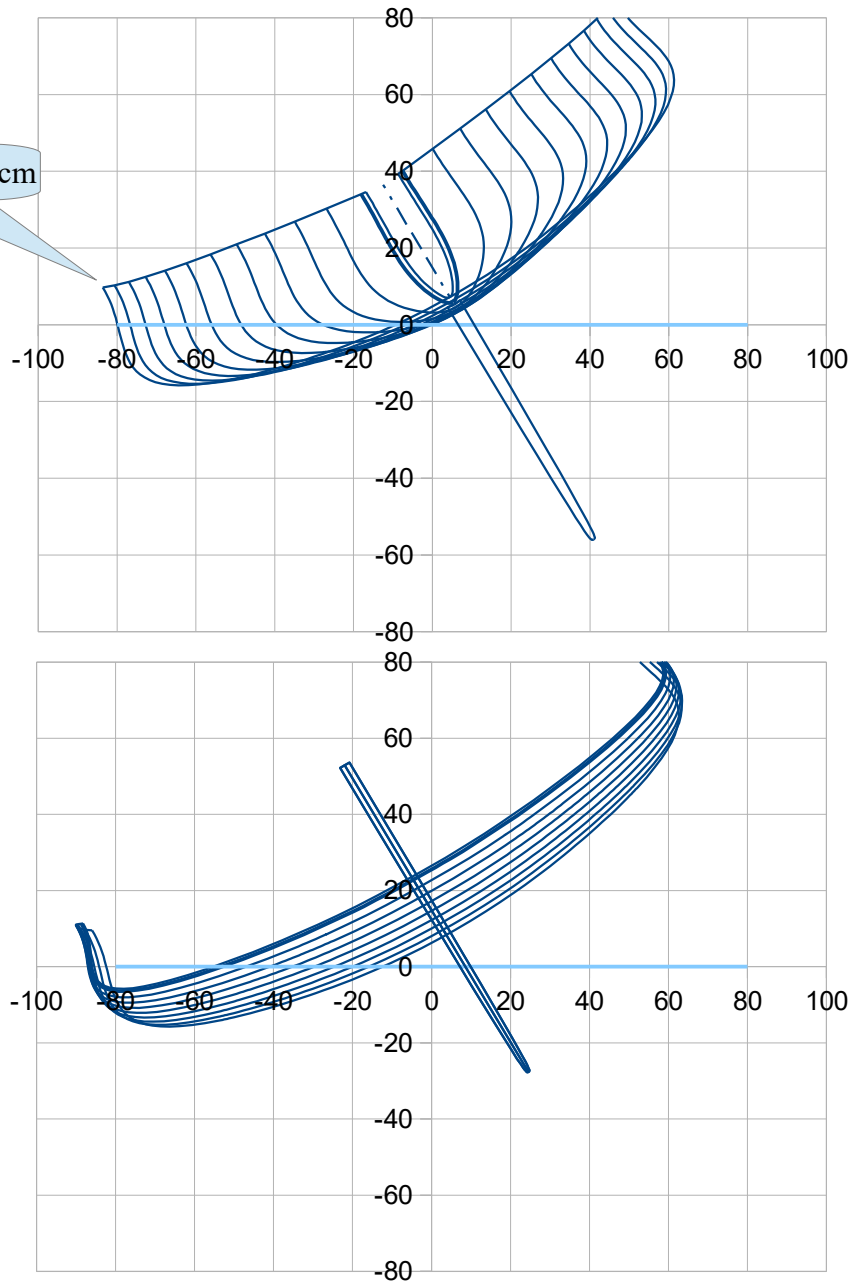
With 10° heel angle :



>>> waterlines have some similarities with Scow ones, although with a more classic bow.

With 30° heel angle : thanks to the volume given by the bump effect, the minimum free-board is still 10 cm :

Free board mini : 10 cm

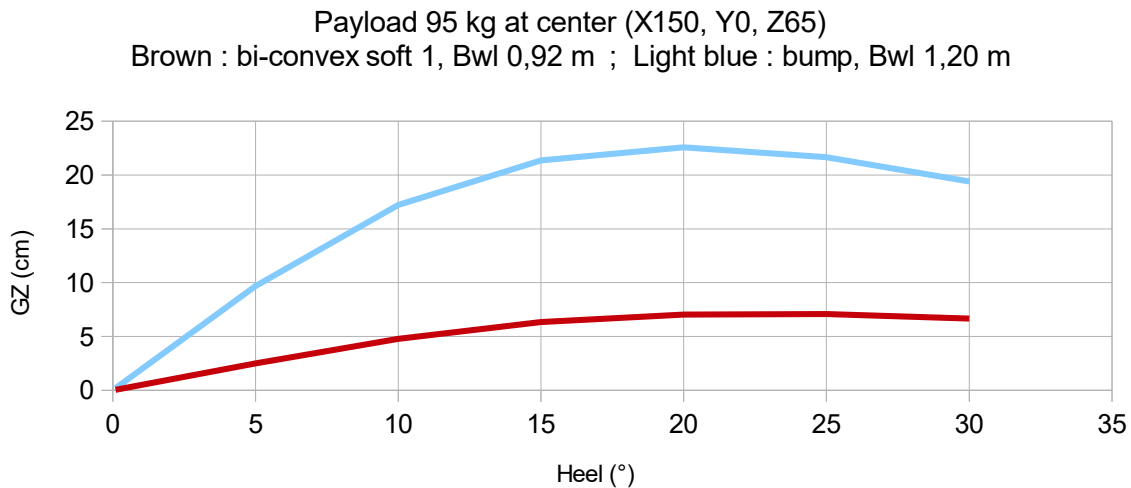


Stability issue when considering the « payload » in the center :

e.g. the helmsman squatted in the boat center under the boom, with his center of gravity at Z +65 cm. It is typically the tack or gybe configuration. Here for the stability comparison it is assumed that the helmsman is (temporarily) fixed like a statue in the center of the boat. and we look at the righting arm GZ evolution for heel up to 25°, due to external action (waves, dynamics of a manoeuvre) and/or due to a transversal offset of the payload.

>>> Comparison with the previous *Bi-convex soft 1* version :

GZ versus Heel

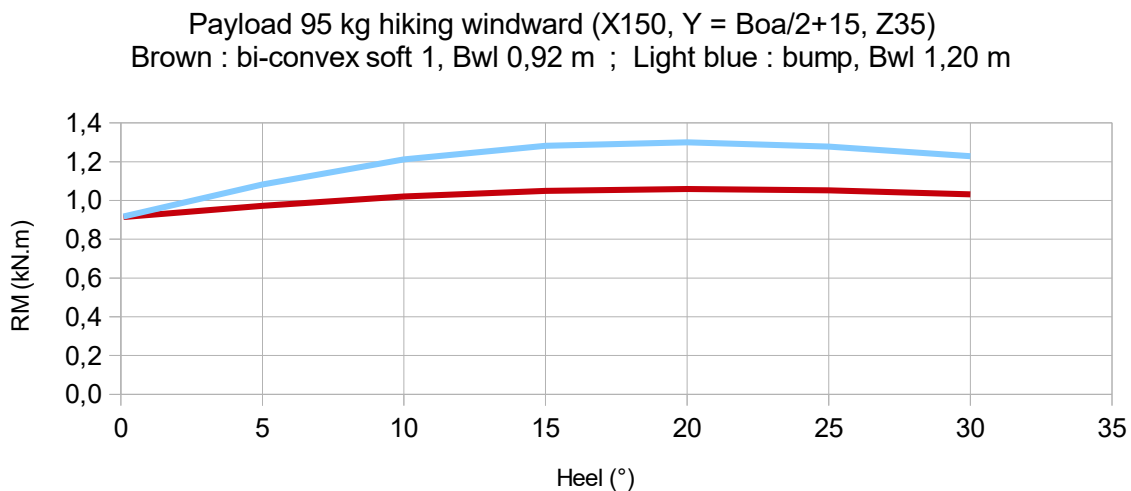


>>> a lot more stability tolerance with the *Bump* option, e.g. at 25° heel angle, a dY offset tolerance for the 95 kg of 39,2 cm / 12,6 cm for the *Bi-convex soft 1*

Righting moment when the « payload » is hiking at windward :

e.g. the helmsman is hiking with its center of gravity estimated at about Y = B/2 + 15 cm and Z = 35 cm (and X still at 150 cm).

Righting moment RM versus Heel

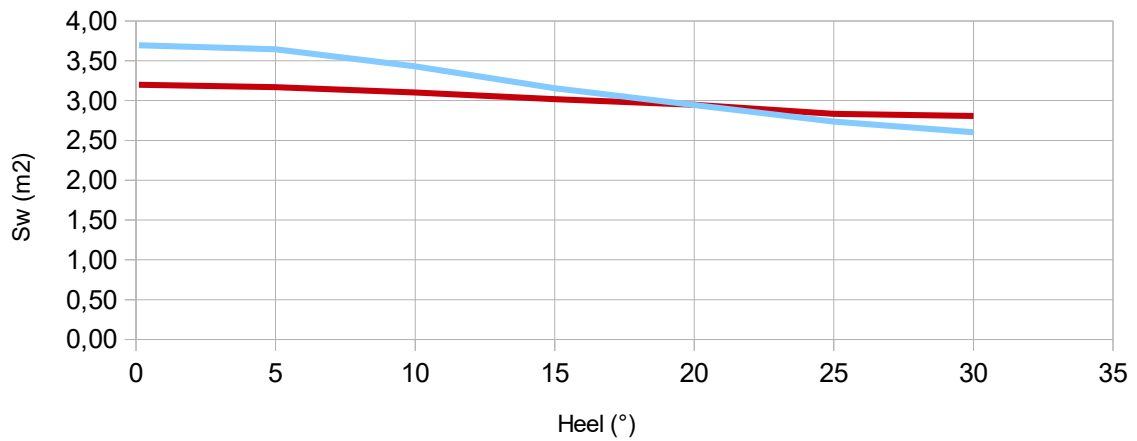


>>> 20% more RM at 10° heel angle thanks to the *Bump* effect

The wetted surface Sw :

Sw versus Heel

Payload 95 kg ; Total Sw inc. daggerboard and rudder
Brown : bi-convex soft 1, Bwl 0,92 m ; Light blue : bump, Bwl 1,20 m



>>> + 15 % Sw for the *Bump* option at low heel angles. The difference becoming 0 at 20° , it is the « Imoca » trend for such hull.

Hydrostatics when upright with payload 95 kg :

2.1 Hull									
Loa (m)	3,97	Lwl (m)	3,75	>Hull speed	4,7	(at Fn 0,4)			
>> ft	13,02		12,30						
B (m)	1,60	at X (% Lwl)	18,0	at sheer line					
>> ft	5,25								
Bwl (m)	1,20	at X (% Lwl)	39,0	> Bwl / B	0,749				
>> ft	3,93			Freeboards (m) >					
Tc (m)	0,094	at X (%Lwl)	50			Aft	Midship	Fore	
>> ft	0,31					0,31	0,37	0,36	
Displacement at H0 (m3)	0,14805	at Xc (m)	1,768	Xc (%Lwl)	47,16	Zc (m)	-0,032		
>> lbs	335	w. seawater	1025	kg/m3		>> ft	-0,10		
Disp at h (cm)	-0,376368726	at Xc (m)	1,778	Xc (%Lwl)	47,42	Zc (m)	-0,004		
Disp at h (cm)	0,376368726	at Xc (m)	1,758	Xc (%Lwl)	46,88	Zc (m)	-0,059		
Cp (%)	54,25								
Sf (m2)	3,08	at Xf (m)	1,634	Xf (%Lwl)	43,57	>>> Xc – Xf (%Lwl)	3,59		
>> ft2	33,17	>> ft	5,36						
Angle immersed sheer li (°)	25,6	at section C4 (40% Lwl)							
Sw (m2)	3,11	>Sw/D^(2/3)	11,10						
>> ft2	33,43								
Shull (m2)	7,29	at X (m)	1,600	Z (m)	0,056				
>> ft2	78,45	>> ft	5,25	>> ft	0,18				
Sdeck (m2)	4,82	at X (m)	1,459						
>> ft2	51,86	>> ft	4,79						
2.2 Daggerboard									
Volume (m3)	0,00282	at X (m)	2,226	X (%Lwl)	59,36	Z (m)	-0,37		
Draft oa (m)	0,80	Sw (m2)	0,30	Sxz (m2)	0,14				
>> ft	2,62	>> ft2	3,24	>> ft2	1,56				
CLR (m)	2,288	CLR (%Lwl)	61,00	method : keel profile extended to the waterline, 25% c at 45% draft oa					
>> ft	7,50								
2.3 Rudder(s)									
Number	1								
Volume (m3)	0,00143	at X (m)	-0,246	X (%Lwl)	-6,57	Z (m)	-0,054		
Sw (m2)	0,18	>> ft	-0,81	Sxz (m2)	0,09	per rudder			
>> ft2	1,92			>> ft2	0,92				
2.4 Hull + Daggerboard + Rudder(s)									
Displacement at H0 (m3)	0,15229	at Xc (m)	1,758	Xc (%Lwl)	46,88	Zc (m)	-0,038		
Disp. (kg)	156,1	>> ft	0,54			>> ft	-0,13		
>> lbs	344								
Sw (m2)	3,58	>Sw/D^(2/3)	12,57	Lwl/D^(1/3)	7,02				
>> ft2	38,58			DLR	82	$M(lbs/2240)/(Lwl(ft)/100)^3$			
2.5 Data from the mass spreadsheet									
Boat with payload	M(kg)	156,1	at Xg (m)	1,564	Xc (%Lwl)	41,71	at Zg (m)	0,576	
Light boat		61,1		1,664				0,461	